

# The identification of a space-dependent load source in anisotropic thermoelastic systems

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## Outline

#### Introduction on thermoelastic systems

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Three types of thermoelasticity							

- ▶  $\Omega \subset \mathbb{R}^d, d \in \{1, 2, 3\}$ : isotropic and homogeneous thermoelastic body
- $\Gamma = \partial \Omega$ : Lipschitz continuous boundary
- ► T: final time
- Coupled thermoelastic system [Muñoz Rivera and Qin, 2002]: specific formulas are used in the study of thermoelasticity to describe how objects change in shape (displacement vector u) with changes in temperature θ from the reference value T<sub>0</sub> > 0 (in Kelvin)

$$\begin{cases} \rho \partial_{tt} \mathbf{u} - \alpha \Delta \mathbf{u} - \beta \nabla (\nabla \cdot \mathbf{u}) + \gamma \nabla \theta &= \mathbf{p} \quad \text{in } \Omega \times (0, T) \\ \rho C_{\mathbf{s}} \partial_t \theta - \kappa \Delta \theta - K * \Delta \theta + T_0 \gamma \nabla \cdot \partial_t \mathbf{u} &= h \quad \text{in } \Omega \times (0, T) \end{cases}$$

- **p**: load (body force) vector; *h*: heat source
- The Lamé parameters α and β, the mass density ρ, the specific heat C<sub>s</sub>, the coupling (absorbing) coefficient γ and the thermal coefficient κ are assumed to be positive constants
- The sign '\*' denotes the convolution product

$$(K * \theta)(\mathbf{x}, t) := \int_0^t K(t - s) \theta(\mathbf{x}, s) \mathrm{d}s, \qquad (\mathbf{x}, t) \in \Omega \times (0, T)$$

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Three types of thermoelasticity							

## Types of thermoelasticity

$$\begin{cases} \rho \partial_{tt} \mathbf{u} - \alpha \Delta \mathbf{u} - \beta \nabla (\nabla \cdot \mathbf{u}) + \gamma \nabla \theta &= \mathbf{p} & \text{in } \Omega \times (0, T);\\ \rho C_s \partial_t \theta - \kappa \Delta \theta - \mathcal{K} * \Delta \theta + \mathcal{T}_0 \gamma \nabla \cdot \partial_t \mathbf{u} &= h & \text{in } \Omega \times (0, T);\\ \mathbf{u}(\mathbf{x}, 0) = \overline{\mathbf{u}}_0(\mathbf{x}), \quad \partial_t \mathbf{u}(\mathbf{x}, 0) = \overline{\mathbf{u}}_1(\mathbf{x}), \quad \theta(\mathbf{x}, 0) &= \overline{\theta}_0(\mathbf{x}) & \text{in } \Omega \end{cases}$$

#### Three types of thermoelasticity:

• type-I: K = 0 and  $\kappa \neq 0$ :

$$\rho C_{s} \partial_{t} \theta - \kappa \Delta \theta + T_{0} \gamma \nabla \cdot \partial_{t} \mathbf{u} = h$$

• type-II:  $K \neq 0$  and  $\kappa = 0$ :

$$\rho C_{s} \partial_{t} \theta - K * \Delta \theta + T_{0} \gamma \nabla \cdot \partial_{t} \mathbf{u} = h$$

• type-III:  $K \neq 0$  and  $\kappa \neq 0$ :

$$\rho C_{\mathsf{s}} \partial_t \theta - \kappa \Delta \theta - K * \Delta \theta + T_0 \gamma \nabla \cdot \partial_t \mathbf{u} = h$$

Inverse source problems for (an-)isotropic thermoelasticity are studied

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literature: inverse source problems for thermoelastic systems								

[Bellassoued and Yamamoto, 2011] investigated an inverse heat source problem for type-I thermoelasticity: they determine h(x) by measuring

$$\mathbf{u}_{|\omega \times (0,T)}$$
 and  $\theta(\cdot, t_0)$ ,



where  $\omega$  is a subdomain of  $\Omega$  such that  $\Gamma \subset \partial \omega$  and  $t_0 \in (0, T)$ 

 [Wu and Liu, 2012] studied an inverse source problem of determining p(x) for type-II thermoelasticity from a displacement measurement

$$\mathbf{u}_{|\omega \times (0,T)|}$$

- Using a Carleman estimate, a Hölder stability for the inverse source problem is proved in both contributions, which implies the uniqueness of a solution to the inverse source problem
- ► Gap: no numerical scheme is provided to recover the unknown source

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### Problem (A)

Can we find a unique  $\mathbf{p}(\mathbf{x})$  and/or  $h(\mathbf{x})$  from the additional final in time measurements

$$\mathbf{u}(\mathbf{x}, T) = \boldsymbol{\xi}_T(\mathbf{x})$$
 and/or  $\theta(\mathbf{x}, T) = \zeta_T(\mathbf{x})$ 

for all types of thermoelasticity and can we provide a numerical scheme?

Goal: The way of retrieving the unknown source is not by the minimization of a certain cost functional (which is typical for IPs), but by using an alternative technique

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## Solution (Problem (A))

Up to now, using our approach, it is possible to recover  $\mathbf{p}(\mathbf{x})$  uniquely for all types of thermoelasticity from the additional final in time measurement (the condition of final overdetermination)

 $\mathbf{u}(\mathbf{x}, T) = \boldsymbol{\xi}_T(\mathbf{x}),$ 

in the presence of a damping term  $\mathbf{g}(\partial_t \mathbf{u})$  in the hyperbolic equation of the thermoelastic system, i.e.

$$\begin{array}{ll} \rho \partial_{tt} \mathbf{u} + \mathbf{g} \left( \partial_{t} \mathbf{u} \right) - \alpha \Delta \mathbf{u} - \beta \nabla \left( \nabla \cdot \mathbf{u} \right) + \gamma \nabla \theta &= \mathbf{p}(\mathbf{x}) & \text{in } \Omega \times (0, T); \\ \rho C_{\mathsf{s}} \partial_{t} \theta - \kappa \Delta \theta - K \ast \Delta \theta + T_{0} \gamma \nabla \cdot \partial_{\mathsf{t}} \mathbf{u} &= 0 & \text{in } \Omega \times (0, T); \\ \mathbf{u}(\mathbf{x}, t) &= \mathbf{0} & \text{on } \Gamma \times (0, T); \\ \theta(\mathbf{x}, t) &= 0 & \text{on } \Gamma \times (0, T); \\ \mathbf{u}(\mathbf{x}, \mathbf{0}) &= \partial_{t} \mathbf{u}(\mathbf{x}, \mathbf{0}) = \mathbf{0}, & \theta(\mathbf{x}, \mathbf{0}) &= \mathbf{0} & \text{in } \Omega, \end{array}$$

 A damping term in thermoelastic systems is also considered in [Qin, 2008, Chapter 9], [Kirane and Tatar, 2001], [Oliveira and Charão, 2008],...

<u>See</u>: Van Bockstal, K. and Slodička, M. *Recovery of a space-dependent vector source in thermoelastic systems.* Inverse Problems in Science and Engineering, 2015, 23, 956–968

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# The results can be extended to anisotropic thermoelastic systems

$$\begin{cases} \varrho(\mathbf{x})\partial_{tt}\mathbf{u} + \mathbf{g}(\partial_{t}\mathbf{u}) + \mathcal{L}^{e}\mathbf{u} + \operatorname{div}(\mathbb{B}(\mathbf{x})\theta) = \mathbf{p}(\mathbf{x}) + \mathbf{r}, & (\mathbf{x}, t) \in \Omega \times (0, T), \\ \varrho(\mathbf{x})C_{s}(\mathbf{x})\partial_{t}\theta - \nabla \cdot (\mathbb{K}(\mathbf{x})\nabla\theta) - (K * \Delta\theta) + T_{0}\mathbb{B}(\mathbf{x}) : \nabla\partial_{t}\mathbf{u} = h, & (\mathbf{x}, t) \in \Omega \times (0, T), \\ \mathbf{u}(\mathbf{x}, t) = \mathbf{0}, & (\mathbf{x}, t) \in \Gamma \times (0, T), \\ \theta(\mathbf{x}, t) = 0, & (\mathbf{x}, t) \in \Gamma \times (0, T), \end{cases}$$

together with the initial conditions

$$\mathbf{u}(\mathbf{x},0) = \mathbf{0}, \quad \partial_t \mathbf{u}(\mathbf{x},0) = \mathbf{0}, \quad \theta(\mathbf{x},0) = 0, \quad \mathbf{x} \in \Omega.$$

As before, the goal is to determine  $\mathbf{p}(\mathbf{x})$  from

$$\mathbf{u}_{\mathcal{T}}(\mathbf{x}) := \mathbf{u}(\mathbf{x}, \mathcal{T}) = \boldsymbol{\xi}_{\mathcal{T}}(\mathbf{x}), \quad \mathbf{x} \in \Omega.$$

<u>See</u>: Van Bockstal, K. and Marin, L. *Recovery of a space-dependent vector source in anisotropic thermoelastic systems.* 

Computer Methods in Applied Mechanics and Engineering, 2017, 321, 269-293

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• Overview results (in both papers):

- A variational approach is used, which implies uniqueness for all types of thermoelasticity if g : ℝ<sup>d</sup> → ℝ<sup>d</sup> is strictly monotone increasing and K is strongly positive definite
- if **g** is linear (i.e.  $\mathbf{g} = g\mathbf{I}$  with g > 0), then
  - A stable iterative algorithm is proposed to recover the unknown vector source p by extending the iterative procedure of [Johansson and Lesnic, 2007] for the heat equation to thermoelastic systems, but without using an adjoint problem
  - It is possible to consider the case of non-homogeneous Dirichlet boundary conditions and initial conditions
  - Also additional given source terms can be considered
- In the following: more details are given for isotropic thermoelasticity of type-III

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Mathematical analysis

Theorem (Well-posedness of the direct problem (given general **p**)) Assume that  $\mathbf{p} : (0, T] \to \mathbf{L}^2(\Omega)$  belong to  $\mathbf{L}^2((0, T), \mathbf{L}^2(\Omega))$ ,  $\overline{\mathbf{u}}_0(\mathbf{x}) \in \mathbf{H}^1(\Omega)$ ,  $\overline{\mathbf{u}}_1(\mathbf{x}) \in \mathbf{L}^2(\Omega)$  and  $\overline{\theta}_0 \in \mathbf{H}^1(\Omega)$ . Assume that any of the following conditions holds for the kernel  $K : (0, T] \to \mathbb{R}$ : (i)  $K'(t) \neq 0$  and  $(-1)^{j}K^{(j)}(t) \ge 0, t > 0, j = 0, 1, 2$ , i.e. K is strongly positive definite; (ii)  $K \in \mathbf{L}^1(0, T)$  s.t.  $\int_0^T |K(t)| dt \le \kappa$ ; (iii)  $\exists C > 0$  s.t.  $\max_{t \in [0, T]} |K(t)| \le C$ . Then, the variational problem has a unique solution  $(\mathbf{u}, \theta)$  such that

$$\begin{split} \mathbf{u} &\in \mathsf{C}\left([0,\,T],\,\mathbf{L}^2(\Omega)\right) \cap \mathsf{L}^2\left((0,\,T),\,\mathbf{H}_0^1(\Omega)\right),\,\partial_t \mathbf{u} \in \mathsf{C}\left([0,\,T],\,\mathbf{L}^2(\Omega)\right),\,\partial_{tt}\mathbf{u} \in \mathsf{L}^2\left((0,\,T),\,\mathbf{H}_0^1(\Omega)^*\right),\\ \theta &\in \mathsf{C}\left([0,\,T],\,\mathbf{L}^2(\Omega)\right) \cap \mathsf{L}^2\left((0,\,T),\,\mathbf{H}_0^1(\Omega)\right) \text{ and } \partial_t \theta \in \mathsf{L}^2\left((0,\,T),\,\mathbf{H}_0^1(\Omega)^*\right). \end{split}$$

Moreover, when  $\overline{u}_0(x) = 0$ ,  $\overline{u}_1(x) = 0$ ,  $\overline{\theta}_0 = 0$ , h = 0 and p = p(x), the following estimate holds

$$\max_{t\in[0,T]}\left\{\left\|\partial_t \mathsf{u}(t)\right\|^2+\left\|\mathsf{u}(t)\right\|_{\mathsf{H}^1_0(\Omega)}^2+\left\|\theta(t)\right\|^2\right\}+\int_0^T\left\|\nabla \theta(t)\right\|^2\mathsf{d} t\leqslant C\left\|\mathsf{p}\right\|^2.$$

 See [Lions and Magenes, 1972] and [Van Bockstal and Marin, 2017, Theorem 4.1]

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Sketch of the proof of uniqueness for type-III thermoelasticity								

Coupled variational formulation: find  $\langle \mathbf{u}(t), \theta(t), \mathbf{p} \rangle \in \mathbf{H}_0^1(\Omega) \times \mathbf{H}_0^1(\Omega) \times \mathbf{L}^2(\Omega)$  such that  $\mathbf{u}(\mathbf{x}, T) = \boldsymbol{\xi}_T(\mathbf{x})$  and

 $\rho\left(\partial_{tt}\mathbf{u},\boldsymbol{\varphi}\right) + \left(\mathbf{g}\left(\partial_{t}\mathbf{u}\right),\boldsymbol{\varphi}\right) + \alpha\left(\nabla\mathbf{u},\nabla\boldsymbol{\varphi}\right) + \beta\left(\nabla\cdot\mathbf{u},\nabla\cdot\boldsymbol{\varphi}\right) + \gamma\left(\nabla\theta,\boldsymbol{\varphi}\right) = \left(\mathbf{p},\boldsymbol{\varphi}\right),\\\rho C_{s}\left(\partial_{t}\theta,\psi\right) + \kappa\left(\nabla\theta,\nabla\psi\right) + \left(k*\nabla\theta,\nabla\psi\right) - \gamma T_{0}\left(\partial_{t}\mathbf{u},\nabla\psi\right) = \mathbf{0},$ 

for all  $\varphi \in \mathsf{H}_0^1(\Omega)$  and  $\psi \in \mathsf{H}_0^1(\Omega)$  and a.a.  $t \in (0, T]$ .

### Theorem (Uniqueness)

Let  $\langle \mathbf{u}_1, \theta_1, \mathbf{p}_1 \rangle$  and  $\langle \mathbf{u}_2, \theta_2, \mathbf{p}_2 \rangle$  satisfy the thermoelastic system. Set  $\mathbf{u} = \mathbf{u}_1 - \mathbf{u}_2$ ,  $\mathbf{p} = \mathbf{p}_1 - \mathbf{p}_2$  and  $\theta = \theta_1 - \theta_2$  such that  $\mathbf{u}(\mathbf{x}, 0) = \mathbf{0}$ ,  $\mathbf{u}(\mathbf{x}, T) = \mathbf{0}$ ,  $\partial_t \mathbf{u}(\mathbf{x}, 0) = \mathbf{0}$  and  $\theta(\mathbf{x}, 0) = 0$ . Then  $\mathbf{p} = \mathbf{0}$  a.e. in  $\Omega$  and  $\langle \mathbf{u}, \theta \rangle = \langle \mathbf{0}, 0 \rangle$  a.e. in  $\Omega \times (0, T)$ .

- Subtract, equation by equation, the variational formulation corresponding with the different solutions
- We want to add up both resulting equation such that the mixed term is cancelled out
- A good choice of the test functions is needed:

$$oldsymbol{arphi} = \partial_t {f u}(t)$$
 and  $\psi = rac{ heta(t)}{{\mathcal T}_0}$ 

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▶ Another trick: integrate in time over (0, *T*) such that

$$\int_{\Omega} \int_{0}^{T} \mathbf{p}(\mathbf{x}) \cdot \partial_{t} \mathbf{u}(\mathbf{x}, t) dt = \int_{\Omega} \left[ \mathbf{p}(\mathbf{x}) \cdot \mathbf{u}(\mathbf{x}, T) - \mathbf{p}(\mathbf{x}) \cdot \mathbf{u}(\mathbf{x}, 0) \right] = 0$$

We obtain that

$$\frac{\rho}{2} \|\partial_t \mathbf{u}(T)\|^2 + \underbrace{\int_0^T \left(\mathbf{g}\left(\partial_t \mathbf{u}_1\right) - \mathbf{g}\left(\partial_t \mathbf{u}_2\right), \partial_t \mathbf{u}_1 - \partial_t \mathbf{u}_2\right)}_{?} + \frac{\rho C_s}{2T_0} \|\theta(T)\|^2 + \frac{\kappa}{T_0} \int_0^T \|\nabla\theta\|^2 + \underbrace{\frac{1}{T_0} \int_0^T \left(K * \nabla\theta, \nabla\theta\right)}_{?} = 0$$

 $\blacktriangleright$  We make distinction based on the different assumptions on K

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# Uniqueness for a Positive Definite Convolution Kernel I

▶ Assume that the twice differentiable function  $K : (0, T] \rightarrow \mathbb{R}$  satisfies

$$\mathcal{K}'(t) 
ot\equiv 0$$
 and  $(-1)^j \mathcal{K}^{(j)}(t) \geqslant 0, \quad t > 0, \quad j = 0, 1, 2,$ 

i.e. K is strongly positive definite

$$\int_0^T \phi(t)(K * \phi)(t) \mathrm{d}t \ge C_0 \int_0^T (K * \phi)^2(t) \mathrm{d}t, \qquad \forall T > 0, \forall \phi \in \mathsf{L}^1_{\mathrm{loc}}(\Omega)$$

This implies

$$\int_{0}^{T} \left( \mathbf{g} \left( \partial_{t} \mathbf{u}_{1} \right) - \mathbf{g} \left( \partial_{t} \mathbf{u}_{2} \right), \partial_{t} \mathbf{u}_{1} - \partial_{t} \mathbf{u}_{2} \right) + \int_{0}^{T} \left\| \nabla \theta \right\|^{2} \leq 0$$

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# Uniqueness for a Positive Definite Convolution Kernel II

Assume g componentwise strictly monotone increasing. Then u<sub>t</sub> = 0 a.e. in Ω × (0, T). Therefore,

$$\mathbf{u}(\mathbf{x},0) = \mathbf{0} \quad \Rightarrow \quad \mathbf{u}(\mathbf{x},t) = \mathbf{0} \text{ a.e. in } \Omega \times (0,T)$$

• 
$$\theta = 0$$
 on  $\partial \Omega \Rightarrow \theta = 0$  a.e. in  $\Omega \times (0, T)$ 

This implies that

$$(\mathbf{p}, oldsymbol{arphi}) = 0, \qquad orall oldsymbol{arphi} \in \mathbf{H}_0^1(\Omega).$$

From this, we conclude that  $\mathbf{p} = \mathbf{0}$  in  $\mathbf{L}^2(\Omega)$ 

Examples:

• E.g. 
$$K(t) = t^{-\alpha}$$
,  $t \in (0, T]$ , with  $0 < \alpha < 1$  (singular kernel)

• E.g.  $K(t) = \exp(-t), t \in [0, T]$ 

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Sketch of the proof of uniqueness for type-III thermoelasticity

# Uniqueness for $K \in L^1(0, T)$ s.t. $\int_0^T |K(t)| dt \leqslant \kappa$ .

Young's inequality for convolutions:

$$\|f * g\|_{r} \leq \|f\|_{p} \|g\|_{q}, \quad \frac{1}{p} + \frac{1}{q} = \frac{1}{r} + 1, \quad 1 \leq p, q, r \leq \infty.$$
 (1)

Applying this inequality, one obtains

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Sketch of the proof of uniqueness for type-III thermoelasticity

# Uniqueness for a bounded convolution kernel

$$\begin{aligned} \left| \int_{0}^{T} \left( \int_{0}^{t} K(t-s) \nabla \theta(s) \mathrm{d}s, \nabla \theta(t) \right) \mathrm{d}t \right| \\ &\leqslant C_{\varepsilon} \int_{0}^{T} \left\| \int_{0}^{t} K(t-s) \nabla \theta(s) \mathrm{d}s \right\|^{2} \mathrm{d}t + \varepsilon \int_{0}^{T} \| \nabla \theta(t) \|^{2} \mathrm{d}t \\ &\leqslant C_{\varepsilon} \int_{0}^{T} \left( \int_{0}^{t} |K(t-s)| \| \nabla \theta(s) \| \mathrm{d}s \right)^{2} \mathrm{d}t + \varepsilon \int_{0}^{T} \| \nabla \theta(t) \|^{2} \mathrm{d}t \\ &\leqslant C_{\varepsilon} \int_{0}^{T} \left( \int_{0}^{t} |K(t-s)|^{2} \mathrm{d}s \right) \left( \int_{0}^{t} \| \nabla \theta(s) \|^{2} \mathrm{d}s \right) \mathrm{d}t + \varepsilon \int_{0}^{T} \| \nabla \theta(t) \|^{2} \mathrm{d}t \\ &\leqslant C_{\varepsilon} \int_{0}^{T} \left( \int_{0}^{t} \| \nabla \theta(s) \|^{2} \mathrm{d}s \right) \mathrm{d}t + \varepsilon \int_{0}^{T} \| \nabla \theta(t) \|^{2} \mathrm{d}t. \end{aligned}$$

Fixing  $\varepsilon$  sufficiently small and applying Grönwall's lemma implies that  $\mathbf{u} = \mathbf{p} = \mathbf{0}$  and  $\theta = 0$ .

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# Algorithm for finding the source term if g is linear

- (*i*) Choose an initial guess  $\mathbf{p}_0 \in \mathbf{L}^2(\Omega)$ . Let  $\langle \mathbf{u}_0, \theta_0 \rangle$  be the solution to the thermoelastic system with  $\mathbf{p} = \mathbf{p}_0$
- (*ii*) Assume that  $\mathbf{p}_k$  and  $\langle \mathbf{u}_k, \theta_k \rangle$  have been constructed. Let  $\langle \mathbf{w}_k, \eta_k \rangle$  solve the thermoelastic system with  $\mathbf{p}(\mathbf{x}) = \mathbf{u}_k(\mathbf{x}, T) \boldsymbol{\xi}_T(\mathbf{x})$

(iii) Define

$$\mathbf{p}_{k+1}(\mathbf{x}) = \mathbf{p}_k(\mathbf{x}) - \omega \mathbf{w}_k(\mathbf{x}, T), \quad \mathbf{x} \in \Omega$$

where  $\omega > 0$  (relaxation parameter), and let  $\langle \mathbf{u}_{k+1}, \theta_{k+1} \rangle$  solve the thermoelastic system with  $\mathbf{p} = \mathbf{p}_{k+1}$ 

- (*iv*) The procedure continues by repeating steps (*ii*) and (*iii*) until a desired level of accuracy is achieved (see next slide)
  - ► This is a Landweber-Fridmann iteration scheme [Fridman, 1956].
  - The proof of convergence can be found in [Van Bockstal and Slodička, 2015, Theorem 3.3] for isotropic materials and in [Van Bockstal and Marin, 2017, Theorem 4.2]

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# Stopping criterion

- Morozov's discrepancy principle is used [Morozov, 1966]
- The case is considered when there is some error in the additional measurement, i.e.

$$\|\boldsymbol{\xi}_{T}-\boldsymbol{\xi}_{T}^{\mathsf{e}}\|\leqslant e,$$

where  $e(\tilde{e})$  depends on the noise level with magnitude  $\tilde{e} > 0$ 

- ▶ The solutions  $\mathbf{p}_k^e$ ,  $\mathbf{u}_k^e$  and  $\theta_k^e$  at iteration k are obtained by using the algorithm
- ► The discrepancy principle suggests to finish the iterations at the smallest index k = k(e, ω) for which

$$E_{k,\mathbf{u}_{T}} = \left\|\mathbf{u}_{k}^{e}(\cdot,T) - \widetilde{\boldsymbol{\xi}}_{T}^{e}\right\| \leq e$$

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## Numerical experiment: setting

- ▶ 1D linear model for isotropic type-I (K = 0) and type-III thermoelasticity is considered
- ▶  $\Omega = [0, 1], T = 1$
- ► copper alloy: shear modulus  $G = 4.8 \times 10^{10} \text{ N/m}^2$ , Poisson's ratio  $\nu = 0.34$ ,  $\alpha_T = 16.5 \times 10^{-6} \text{ }^{1}\text{/K}$ ,  $\kappa = 401 \text{ }^{W}\text{/mK}$ ,  $\rho = 8960 \text{ }^{\text{kg}}\text{/m}^3$  and  $C_s = 385 \text{ }^{J}\text{/kgK}$
- $g = 2 \times 10^8$ ,  $T_0 = 293 {
  m K}$

• 
$$\alpha = \mu$$
,  $\beta = \mu + \lambda$  with  $\lambda = \frac{2\nu G}{1 - 2\nu}$  and  $\mu = G$ 

► Three choices for the convolution kernel are made, namely K = 0,  $K = \exp(-t)$  and  $K = 1/\sqrt{t}$ 

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## Numerical experiment: setting

- The forward coupled problems in this procedure are discretized in time according to the backward Euler method with timestep 0.0005
- At each time-step, the resulting elliptic coupled problems are solved numerically by the finite element method (FEM) using first order (P1-FEM) Lagrange polynomials for the space discretization. A fixed uniform mesh consisting of 200 intervals is used



The finite element library DOLFIN [Logg and Wells, 2010, Logg et al., 2012b] from the FEniCS project [Logg et al., 2012a] is used

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Results of numerical experin	nents				

Exact solution

$$u(x,t) = (1+t)^2 x(x-1)^2$$
 and  $\theta(x,t) = (1+t)x(1-x)^2$   
 $p_1(x) = 10x(1-x)$ 



Figure: The exact source  $p_1$  and its corresponding numerical solution, retrieved using various levels of noise in the additional measurement, for various convolution kernels, namely (a) K = 0, (b)  $K = \exp(-t)$ , and (c)  $K = 1/\sqrt{t}$ . The relaxation parameter  $\omega = 10$ .

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$$p_2(x) = \exp\left(-20(x-0.5)^2
ight)$$



Figure: The exact source  $p_2$  and its corresponding numerical solution, retrieved using various levels of noise in the additional measurement, for various convolution kernels, namely (a) K = 0, (b)  $K = \exp(-t)$ , and (c)  $K = 1/\sqrt{t}$ . The relaxation parameter  $\omega = 10$ .

Thermoelastic systems OO O	Problem 0000	Uniqueness 00 <b>0</b> 00	Algorithm 00	Numerical Experiments	Conclusion and further research
Results of numerical experime	nts				

Table: The stopping iteration number  $\tilde{k} = k(e(\tilde{e}), 10)$  and the CPU time (mins), obtained for the experiments with the unknown sources  $p_1$  and  $p_2$ .

ẽ		1%	p	1 5%		10%	0	.5%	1	P2 L%	:	3%
	Ĩĸ	time	ĩ	time	ĥ	time	ĩ	time	ĩ	time	ĩ	time
<i>K</i> = 0	136	94.7	11	8.2	9	6.3	387	327.4	386	327.2	172	60.7
$K = \exp(-t)$	133	138.7	9	10.4	9	9.9	503	538.1	321	416.2	177	111.2
$K = 1/\sqrt{t}$	142	144.3	10	11	8	8.9	491	532.6	390	468.4	206	183.4

Following experiments:

$$p_{3}(x) = \begin{cases} 0 & 0 \leqslant x \leqslant \frac{1}{3} \\ 6x - 2 & \frac{1}{3} \leqslant x \leqslant \frac{1}{2} \\ 4 - 6x & \frac{1}{2} \leqslant x \leqslant \frac{2}{3} \\ 0 & \frac{2}{3} \leqslant x \leqslant 1 \end{cases} \quad p_{4}(x) = \begin{cases} x(0.5 - x)(1 - x) & 0 \leqslant x \leqslant \frac{1}{2} \\ x(x - 0.5)(1 - x) & \frac{1}{2} \leqslant x \leqslant 1 \end{cases}$$
$$p_{5}(x) = \begin{cases} 0 & 0 \leqslant x < \frac{1}{3} \\ 1 & \frac{1}{3} \leqslant x \leqslant \frac{2}{3} \\ 0 & \frac{2}{3} < x \leqslant 1 \end{cases} \quad p_{6}(x) = 10x(x - 1)^{2}$$

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Figure: The exact sources  $p_3$ ,  $p_4$  and  $p_5$  and its numerical approximations for  $\tilde{e} = 0\%$  (a,c,e) and for different noise levels (b,d,f). The relaxation parameter  $\omega = 10$ .

Thermoelastic systems	Problem	Uniqueness	Algorithm	Numerical Experiments	Conclusion and further research
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## Other relaxation parameter



Figure: The exact source  $p_4$  and its numerical approximations for  $\omega = 2$  (a) and for  $\omega = 20$  (b).

• The results for small noise are similar to the results obtained when  $\omega = 10$ 

Thermoelastic systems 00 0	Problem 0000	Uniqueness 00000	Algorithm 00	Numerical Experiments	Conclusion and further research 00 <b>0</b>



Figure: The exact source  $p_5$  and its numerical approximations for  $\tilde{e} = 1\%$  (a) and for  $\tilde{e} = 3\%$  (b) for different values of g. The relaxation parameter  $\omega = 10$ .



Figure: The exact source  $p_2$  and its numerical approximations for  $\tilde{e} = 3\%$  for different values of g. The relaxation parameter  $\omega = 10$ .

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Figure: The non-symmetric exact source  $p_6$  and its numerical approximations (using  $\tilde{e} = 3\%$ ) for different initial guesses: 0 (a),  $6.44x - 12.27x^2 + 5.83x^3$  (b),  $9.68x - 18.46x^2 + 8.78x^3$  (c) and  $12.88x - 24.54x^2 + 11.65x^3$  (d). The relaxation parameter  $\omega = 10$ .

Thermoelastic systems 00 0	Problem 0000	Uniqueness 00000	Algorithm 00	Numerical Experiments ○○ ○○○○○○●	Conclusion and further research 00 <b>0</b>	
Results of numerical experiments						



Figure: The non-symmetric exact source  $p_6$  and its numerical approximations for T = 0.2 (a) and T = 0.5 (b). The relaxation parameter  $\omega = 10$ .

Thermoelastic systems	Problem	Uniqueness	Algorithm	Numerical Experiments	Conclusion and further research
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## Conclusion

- It is possible to recover uniquely an unknown vector source in all types of damped thermoelastic systems when an additional final in time measurement of the displacement is measured
- A numerical algorithm in a linear case gives accurate shape recovery
- ▶ The algorithm is sensitive to the amount of noise added to the data
- There is a certain limitation of the method with respect to the recovery of non-symmetric sources

Thermoelastic systems	Problem	Uniqueness	Algorithm	Numerical Experiments	Conclusion and further research
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## Future research

- More numerical experiments (e.g. influence of the parameter g on the results)
- Testing different stopping criteria (up to now, no better results)
- ▶ What if **g** is nonlinear?
- Other inverse problems for thermoelasticity, e.g. the recovery of time-dependent sources, convolution kernel
- ▶ Goal: with numerical scheme!

Thermoelastic systems	Problem	Uniqueness	Algorithm	Numerical Experiments	Conclusion and further research
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Thermoelastic systems	Problem	Uniqueness	Algorithm	Numerical Experiments	Conclusion and further research
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